

A reliable,
user-friendly
tool, according
to Eurocodes

GEOFOND

Shallow and deep foundations design

Calculation of settlements under embankments



AN EASY AND RELIABLE ANALYSIS

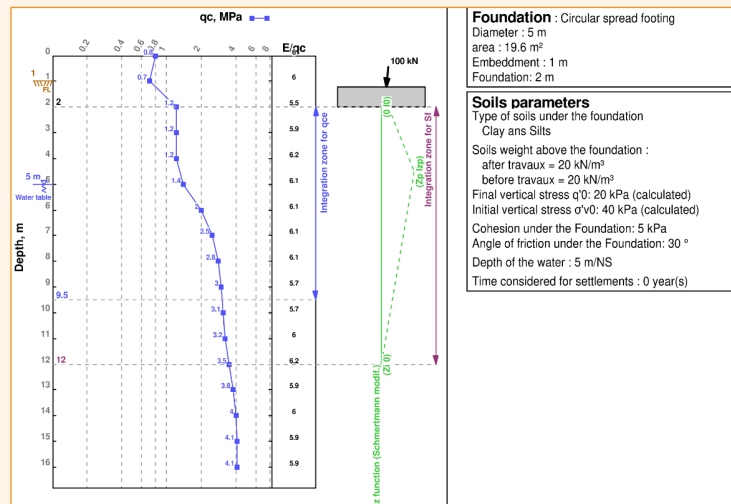
- **Foundations:** bearing capacities and settlements
- **Embankments:** punching failure safety factors and oedometric and elastic settlements under embankments



Source : Vinci

A DESIGN ACCORDING TO EUROCODES

- **Shallow foundations**
- **Deep foundations:** piles, pile groups, rigid inclusions and ballast piers
- Simple and complex **embankments**



ADAPTED CALCULATION TOOLS

- **Consideration of a wide range of tests:** pressuremeter, oedometer, penetrometer, laboratory tests
- Various design methods: **Schmertmann, Meyerhof, Burland...**

Choice of French standards: **NF P 94-261** (shallow foundations)
➤ and **NF P 94-262** (deep foundations), **DTU, Fascicule 62-Chapter V**

ADVANCED ANALYSIS OPTIONS

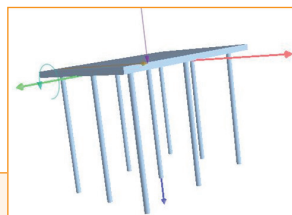
- Piles under **horizontal charges**
- Group of **piles design**, considering torsion in the head of distribution structure
- Calculation of **negative skin friction:** fascicule 62 and norm NF P 94-262
- Verification of concrete efforts

Calculation results: Bearing capacity

With the NF P 94-262 method
 $R_s = 0.881 \text{ MN}$ Ann. F.5
 $P_{le} = 0.522 \text{ MPa}$ Ann. F4.2.3 $k_{pmax} = 1.1$ Tab. F4.2.1
 $Def = 5.71 \text{ m}$ $k_p = 1.1$ Ann. F4.2
 $q_b = 0.574 \text{ MPa}$ Ann. F4.2.1 $R_b = 0.162 \text{ MN}$ Ann. F4.1

Check on the characteristics of the material conc

$k_1 = 1.3, k_2 = 1, k_3 = 1$ $c_{max} = 35 \text{ MPa}$
 $f_{ck}^* = 7.69 \text{ MPa}$
 $\sigma_{avgSLS} = k_3 * 0.3 * f_{ck}^* = 2.31 \text{ MPa}$
 $\sigma_{maxSLS} = \min(0.6 * f_{ck}^*, 0.6 * f_{ck}^*) = 4.62 \text{ MPa}$
 $N_{avgSLS} = \sigma_{avgSLS} * A = 0.652 \text{ MN}$



Calculation results : settlements

Under a stress $q_{ref} = 1.96 \text{ MPa}$
 With the Frank & Zhao method.
 $q(7.5) = 574 \text{ kPa}$
 $qp(7.5) = 293 \text{ kPa}$
 $q'u(7.5) = 82.9 \text{ kN}$
 Settlement $D = 3.91 \text{ mm}$

Calculation results : skin friction

On an isolated element
 $G_{sn}(inf) = 2827 \text{ kN}$
 $h_1 = 7.5 \text{ m}$ et $h_2 = 7.5 \text{ m}$ (defined in the data) /NS
On an element within a group
 $G_{sn}(b) = 99.95 \text{ kN}$ with $b=0.564 \text{ m}^2$ et $G_{sn}(b)$ bounded = 150 kN
 $h_1 = 0.8 \text{ m}$ et $h_2 = 7.5 \text{ m}$ (defined in the data) /NS
 skin friction on the angle elements
 $G_{sna} = 7/12 * G_{sn}(b) + 5/12 * G_{sn}(inf) = 1236 \text{ kN}$
 skin friction on the elements at the border of the group
 $G_{sne} = 5/6 * G_{sn}(b) + 1/6 * G_{sn}(inf) = 554.5 \text{ kN}$
 skin friction on the elements within the group
 $G_{sni} = G_{sn}(b) = 99.95 \text{ kN}$

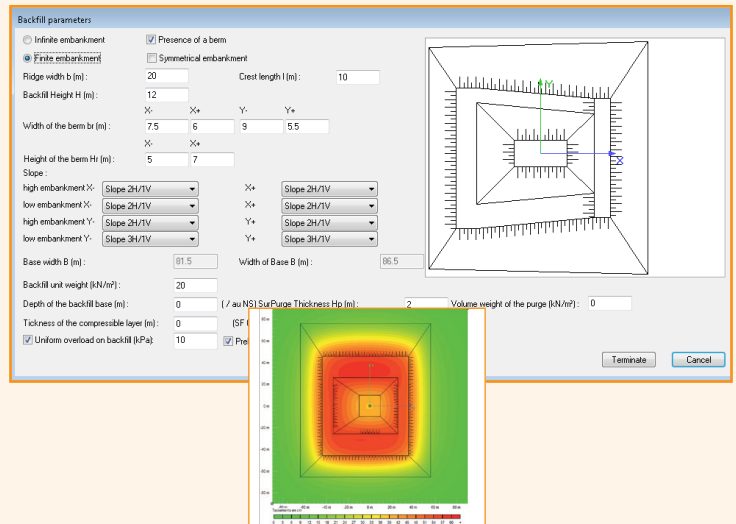


OPTIMIZATION MODULES

- **Deterministic calculation** with an analysis variable choice: Influence of foundation dimensions on bearing capacities, or influence of charges on settlements
- **Probabilistic calculation** with consideration of uncertainty

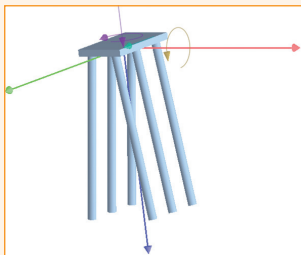
COMPLEX EMBANKMENT DESIGN

- **Finite or infinite embankments**
- Elastic and oedometric settlements on different time lapses
- Consideration of **non-symmetric geometries and berms**
- Graphic display of settlements **isovalues**
- **Stresses and settlements variation** curves, depending on the depth



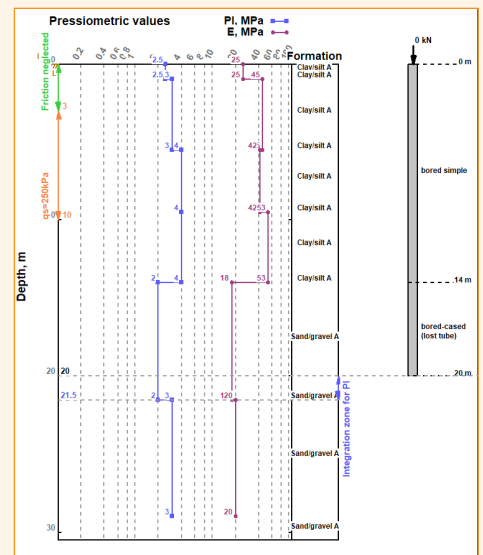
BALLAST PIERS AND RIGID INCLUSIONS DESIGN

- Determination of the bearing capacity according to **COPREC-SOFFONS** recommendations
- Stresses verification according to **PRIEBE** and **FHWA** methods (Federal Highway Administration - USA)



PILE GROUP MODULE

- Pile and footing **displacements**
- **Efforts, moments and maximal displacements in each pile**
- **Tridimensional** display of pile groups



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